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# Programmed Energy Dispersive X-Ray Analysis of Top Coats of Automotive Paint 

Elemental analysis is a necessary approach to the characterization of physical evidence in forensic science laboratories [1]. There are many wet chemical and instrumental methods in use; however, with few exceptions, these techniques are difficult to apply, have considerable sample size or preparation constraints, are time consuming, or are destructive. Energy dispersive X-ray (EDX) spectrometry does not have these disadvantages [2,3].

The analytical system used in this study is EDX spectrometry in conjunction with a minicomputer capable of sorting numerous emission energies and furnishing output on either a cathode ray tube (CRT) or a teletype. The emission energies displayed on the CRT represent the elemental composition of the material $[3,4]$.

The forensic analysis of paint samples generally requires time-consuming analytical techniques. Samples that cannot be differentiated by obvious physical properties should be compared on the basis of their organic and inorganic chemical composition before a final conclusion is reached [5]. This study is concerned with the inorganic composition of the paint samples and in particular with a technique that rapidly and nondestructively determines the elemental composition of paint samples for comparisons. Any technique that can do this is invaluable in a forensic science laboratory [ $5, \mathrm{p} .138$ ].

After examining the results of a study [6] that compared the ability of emission spectrography and EDX to differentiate automotive paints, the authors decided to develop an automated technique for the EDX analysis of automotive paint samples.

In 1974, the U.S. National Bureau of Standards (NBS) Law Enforcement Standards Laboratory prepared and distributed a standard reference collection of 140 American automotive surface coatings used in 1974 entitled Automotive Colors to forensic science laboratories throughout the United States. The paint standards represent those types that were new for the model year or were carried over from previous years. Further information in the collection included sample number, metallic or nonmetallic flaking texture, manufacturer reference number, and automobile make and model using the paint color. All the top coats in this collection were prepared from production line batches sprayed on aluminum or paper sheets. The painted sheets were compared visually and instrumentally against master color standards and then cut into 25 by $40-\mathrm{mm}$ samples. For these reasons it was decided that analytical results from the collection would

[^0]interest the forensic science community, and the automated technique developed for EDX was demonstrated by the analysis of these standard paint samples.

The authors determined the elemental composition of these paint samples and tabulated the data (Table 1). Matters outlined include operating conditions, comparison of sample data, evaluation of EDX spectrometer stability, homogeneity of samples, and homogeneity of corresponding paint samples from different NBS Automotive Colors collections.

## Method

Samples from the NBS collection were analyzed for inorganic components, both qualitatively and semiquantitatively, by using a Finnigan 900F EDX spectrometer. Preliminary work established the optimum conditions for analyzing the paint standards. All the paint samples were prepared for analysis by removing them from their holding frames and placing them on the rotating sample tray in the X-ray cavity.
The instrument conditions used were 31.0 to 35.0 kV and 4.00 mA for the excitation energies of the rhodium X-ray tube with dead time of 35 to $40 \%$ on the analog-to-digital converter (ADC). The samples were irradiated in an air path using a rhodium filter and indium collimator. Although bremsstrahlung radiation was increased with these operating conditions the detection of the heavier elements was improved. The indium collimator was used for two reasons: it has an absorption edge higher than most elements detected and the short ( $1.6-\mathrm{mm}$ ) collimator allowed the detector to receive emissions from a broad area of the specimen. If lightweight paint chips (approximately $50 \mu \mathrm{~g}$ ) or small areas (approximately $0.25 \mathrm{~mm}^{2}$ ) are to be examined, the longer molybdenum collimator has to be used and the samples have to be prealigned with the collimator.

Initial testing disclosed that the paint standards are divided into four main categories defined by the predominant elemental peak: iron, barium, titanium, and lead. Occasionally, a different category was observed (calcium or strontium), but this was infrequent and these exceptions were not separately categorized.

Most of the paint specimens on aluminum sheets exhibited the presence of copper which was attributed to electrolytically deposited copper on the backing between the aluminum sheet and the sprayed paint. The copper deposit was observed visually, and paint samples that were affected are indicated by an asterisk in Table 1. Approximately $75 \%$ of the paint samples were mounted on aluminum backings. The backing was sufficiently excited by the X-ray beam to interfere with analysis. A spectrum stripping technique to overcome this problem has been evaluated and is considered in greater detail in a later portion of this study. Those samples with aluminum backing without the electrolytically deposited copper are indicated by two asterisks in Table 1.

Certain elements were common to many of the samples (Table 2). Each sample was analyzed automatically for 12 elements by programming the $16-\mathrm{K}$ core computer of the EDX system. Observation of the areas of selected elemental peaks and differentiation of background counts from peak area counts were performed as indicated in Fig. 1. A total of 512 channels in each half of the memory core retained energy pulses received from the detector. When an element was present, its particular energy pulses were directed to the corresponding channels in the vicinity of the channel defined as the peak centroid (peak ID) (Fig. 1) and the pulses were counted and stored for tabulation and display.

A width of eleven channels was designated in the program, with the center channel superimposed on the peak ID. Five channels spanned each side of the peak ID in a symmetrical fashion. This channel width was sorted and counted, irrespective of peak size, by following routine channel calibration procedures. Right and left spans for defining the background area beneath each peak were established to create as consistent a
TABLE 1-Elemental composition of automotive paints used in 1974. ${ }^{a}$

| Sample | Metallic Paint | Counting Time, s | Ca | Ti-Ka/ $\mathrm{Ba}-\mathrm{L}_{\alpha}$ Ratio | $\begin{gathered} {\mathrm{Ti} i-\mathrm{K}_{\beta} /}^{\text {Ba-L }} \\ \text { Ratio } \end{gathered}$ | Cr | Mn | Cu | Zn | $\begin{gathered} \text { As-L } L_{a} / \\ \text { Pb-La } \\ \text { Ratio } \end{gathered}$ | Se-Ka | As-L ${ }_{\beta} /$ $\mathrm{Br}-\mathrm{K}_{\alpha}$ Ratio | $\mathrm{Pb}-\mathrm{L}_{\rho} /$ <br> $\mathrm{Se}-\mathrm{K}_{\boldsymbol{\beta}}$ <br> Ratio | Sr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Iron-Based Paints |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| B0051** | yes | 67 | 0.003 | 0.364 | 0.068 | 0.009 | 0.607 | 0.305 | ... | $\ldots$ | $\ldots$ | 0.004 | 0.012 | 0.018 |
| B0052 | yes | 144 | 1.13 | 0.857 | 0.148 |  |  |  | 0.548 |  |  |  |  | 0.122 |
| B0092* | yes | 82 | ... | 0.002 | 0.003 | 0.188 | 0.920 | 0.546 | 0.388 | ... | $\ldots$ | 0.033 | 0.010 | 0.051 |
| B0129** | yes | 77 | ... | 0.007 | ... | 0.292 | 0.919 | 0.537 | 0.256 | 0.003 |  | 0.008 | 0.031 | 0.044 |
| C0041 | no | 155 | 1.12 | 1.00 | 0.184 |  |  |  | 0.567 | 0.005 | $\ldots$ | ... |  | 1.05 |
| C0080** | yes | 74 | 0.004 | 0.404 | 0.056 | 0.023 | 0.797 | 0.431 | . ... | ... | $\ldots$ | $\ldots$ | $\ldots$ | 0.029 |
| C0090* | no | 70 |  | ... | ... | 0.136 | 0.728 | 0.495 | 0.178 | 0.006 | ... | $\ldots$ | $\ldots$ | 0.028 |
| E0068 | yes | 44 | 0.238 | 0.374 | 0.071 | 0.021 | 0.001 |  | 0.111 | ... | $\ldots$ | ... |  | 0.075 |
| E0085** | yes | 44 | ... | 0.248 | 0.037 | 0.011 | 0.470 | 0.224 | ... | $\ldots$ | $\ldots$ | $\ldots$ | 0.031 | 0.022 |
| E0130* | yes | 40 | ... | ... | ... | 0.070 | 0.387 | 0.218 | 0.023 |  | $\ldots$ |  | 0.001 | 0.029 |
| F0009* | yes | 23 | 0.002 | 0.486 | 0.404 | 0.076 | 0.109 | 0.057 | 0.024 | 0.198 | ... | 0.002 | 0.142 | 0.122 |
| F0012* | yes | 27 | 0.008 | 0.353 | 0.276 | 0.069 | 0.220 | 0.098 | 0.005 | 0.009 | $\ldots$ | ... | 0.002 | 0.048 |
| F0013** | yes | 14 | 0.004 | 0.271 | 0.194 | 0.034 | 0.073 | 0.033 | 0.009 | ... | $\ldots$ | ... | ... | 0.061 |
| F0025* | yes | 14 | ... | 0.204 | 0.154 | 0.027 | 0.090 | 0.032 | 0.020 | $\ldots$ | $\ldots$ | ... | ... | 0.051 |
| F0031** | yes | 21 | 0.001 | 0.430 | 0.378 | 0.043 | 0.110 | 0.054 | 0.343 | 0.017 | $\ldots$ | $\cdots$ | 0.014 | 0.188 |
| F0032** | yes | 35 | ... | 0.851 | 0.768 | 0.112 | 0.174 | 0.086 | 0.746 | 0.005 | $\ldots$ |  | $\ldots$ | 0.336 |
| F0038** | yes | 19 | ... | 0.444 | 0.422 | 0.051 | 0.072 | 0.039 | 0.328 | 0.006 | $\ldots$ |  |  | 0.208 |
| F0039** | yes | 29 | ... | 0.628 | 0.546 | 0.074 | 0.144 | 0.096 | 0.550 | 0.022 | $\ldots$ | 0.054 | 0.009 | 0.272 |
| F0040** | yes | 14 | 0.006 | 0.268 | 0.244 | 0.033 | 0.061 | 0.024 | 0.270 |  |  |  |  | 0.128 |
| F0047 | yes | 30 | 0.186 | 0.320 | 0.048 | ... | 0.005 | ... | 0.078 |  | $\ldots$ | 0.052 | $\ldots$ | 0.027 |
| Fous9 | yes | 28 | 0.15'1 | 0.274 | 0.046 | ... | 0.007 | $\ldots$ | 0.080 | 0.005 | ... | ... | .. | 0.103 |
| F0062 | yes | 52 | 0.324 | 0.555 | 0.097 | ... | ... | ... | ... | 0.148 | $\ldots$ | $\ldots$ | 0.016 | 0.051 |
| F0071 | yes | 157 | 1.28 | 0.960 | 0.165 | ... | $\ldots$ | $\ldots$ | 0.573 |  | $\ldots$ | $\ldots$ | ... | 0.250 |
| F0074 | yes | 35 | 0.241 | 0.197 | 0.039 | 0.006 | 0.003 | $\ldots$ | 0.097 | 0.019 | $\ldots$ | $\ldots$ | $\ldots$ | 0.019 |
| F0075 | yes | 65 | 0.391 | 0.812 | 0.136 | $\ldots$ | ... |  | 0.157 |  |  | $\ldots$ | 0.008 | 0.092 |
| F0077* | yes | 76 | ... | 0.375 | 0.058 | 0.020 | 0.702 | 0.342 | ... | 0.189 | $\ldots$ | $\ldots$ | 0.189 | $\cdots$ |
| F0078* | no | 21 | ... | 0.456 | 0.071 | 0.007 | 0.159 | 0.112 | ... | ... | ... | $\ldots$ | ... | 0.038 |
| F0082** | yes | 36 | $\ldots$ | 0.226 | 0.036 | 0.009 | 0.361 | 0.206 | $\cdots$ | 0.008 | $\ldots$ | 0.008 | $\ldots$ | 0.044 |
| F0084 | yes | 1559 | 1.35 | 0.184 | . | . | . | . | 0.593 | ... | $\ldots$ | ... | $\ldots$ | 0.230 |
| F0089** | yes | 56 | ... | 0.143 | 0.014 | 0.004 | 0.512 | 0.288 | 0.019 | $\ldots$ | $\ldots$ | $\ldots$ | ... | 0.024 |
| F0109** | yes | 27 | $\cdots$ | 0.396 | 0.249 | 0.032 | 0.169 | 0.103 | 0.038 | $\ldots$ | $\ldots$ | $\ldots$ | 0.008 | 0.080 |

TABLE 1-Continued.

| Sample | Metallic Paint | Counting Time, s | Ca | $\begin{aligned} & \mathrm{Ti}-\mathrm{K}_{a} / \\ & {\mathrm{Ba}-\mathrm{L}_{\alpha}}^{\text {Ratio }} \end{aligned}$ | $\begin{aligned} & \mathrm{Ti}-\dot{K}_{\beta} / \\ & \text { Ba-L }_{\beta} \\ & \text { Ratio } \end{aligned}$ | Cr . | Mn | Cu | Zn | $\begin{aligned} & \text { As- } \mathrm{L}_{\alpha} / \\ & \mathrm{Pb}-\mathrm{L}_{\alpha} \\ & \text { Ratio } \end{aligned}$ | $\mathrm{Se}-\mathrm{K}_{\text {a }}$ | $\begin{aligned} & \text { As-L्/ } / \\ & \mathrm{Br}-\mathrm{K}_{\alpha} \\ & \text { Ratio } \end{aligned}$ | $\mathrm{Pb}-\mathrm{L}_{\beta} /$ $\mathrm{Se}-\mathrm{K}_{\beta}$ Ratio | Sr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| F0110* | yes | 21 | ... | ... | ... | 0.067 | 0.221 | 0.146 | 0.042 | 0.003 | . |  |  |  |
| F0111* | yes | 18 | ... | 0.018 | ... | 0.031 | 0.171 | 0.093 | 0.021 | ... | 0.037 | 0.017 | ... |  |
| F0112* | no | 37 | 0.005 | 0.899 | 0.145 | 0.042 | 0.314 | 0.196 | 0.052 | ... | . | 0.014 |  | 0.033 |
| F0113* | yes | 11 | ... | 0.003 | ... | 0.031 | 0.107 | 0.049 | 0.040 | ... | ... | . | . . . | 0.007 |
| F0114* | no | 20 | $\ldots$ | 0.456 | 0.060 | 0.038 | 0.161 | 0.115 | 0.022 | . . . | ... | $\ldots$ | ... | 0.014 |
| F0116* | yes | 46 | 0.004 | ... | ... | 0.093 | 0.470 | 0.337 | 0.133 | $\ldots$ | . |  | ... | 0.014 |
| F0126* | yes | 54 | ... | 0.010 | 0.004 | 0.200 | 0.572 | 0.342 | 0.213 | ... | $\cdot$ | 0.151 | $\ldots$ | 0.026 |
| F0127* | yes | 36 | $\ldots$ | ... | ... | 0.096 | 0.386 | 0.200 | 0.186 | 0.007 | $\ldots$ | 0.017 | . |  |
| F0128* | yes | 52 | $\ldots$ | 0.003 | . $\cdot$ | 0.170 | 0.542 | 0.416 | 0.069 | ... | ... | ... |  |  |
| F0133* | yes | 11 | $\ldots$ | ... | ... | 0.021 | 0.096 | 0.066 | 0.016 | 0.012 | . $\cdot$ |  | 0.002 | 0.004 |
| F0134* | yes | 55 | 0.003 | 0.004 |  | 0.061 | 0.417 | 0.276 | 0.095 | ... | $\ldots$ | 0.019 | 0.029 | 0.012 |
| F0137* | yes | 21 | 0.001 | 0.003 | 0.004 | 0.087 | 0.230 | 0.121 | 0.051 | ... | $\ldots$ | . . . | 0.005 | 0.010 |
| F0138* | yes | 10 | 0.004 | 0.005 | 0.006 | 0.018 | 0.102 | 0.044 | 0.015 | ... | $\ldots$ | ... |  |  |
| F0139* | yes | 55 | ... | ... | ... | 0.160 | 0.612 | 0.401 | 0.073 | ... | ... | ... |  | 0.035 |
| G0088** | yes | 20 | ... | 0.064 | 0.011 | 0.004 | 0.180 | 0.192 | 0.014 | ... | $\ldots$ | ... | 0.012 |  |
| H0036* | no | 27 | ... | 0.911 | 0.370 | 0.036 | 0.165 | 0.074 | 0.042 | ... | 0.004 |  | 0.008 | 0.079 |
| H0048* | yes | 55 | $\ldots$ | 0.382 | 0.059 | 0.016 | 0.482 | 0.241 | . . | ... | . | 0.011 |  | 0.046 |
| H0066* | no | 19 | . | 0.405 | 0.068 | 0.001 | 0.172 | 0.116 | . . | ... | ... | . | 0.021 | 0.020 |
| H0086** | yes | 66 | 0.005 | 0.470 | 0.083 | 0.016 | 0.690 | 0.434 | . | . | ... | $\ldots$ |  | 0.028 |
| H0117* | no | 9 | ... | 0.124 | 0.014 | 0.048 | 0.081 | 0.044 | 0.012 | 0.310 | . . | . . . | 0.218 |  |
| H0118* | no | 48 | . | - | . | 0.098 | 0.520 | 0.376 | 0.122 |  |  |  |  |  |
| H0120** | no | 30 | 0.003 | 0.730 | 0.123 | 0.086 | 0.280 | 0.157 | 0.081 | 0.014 | 0.002 | 0.012 | 0.019 | 0.005 |
| J0028** | yes | 17 | 0.003 | 0.348 | 0.288 | 0.043 | 0.093 | 0.061 | 0.328 | 0.012 | 0.001 | 0.038 | 0.007 | 0.113 |
| J0105* | yes | 39 | 0.105 | 0.027 | 0.009 | 0.143 | 0.462 | 0.234 | 0.114 | . . | . | 0.025 | . . | 0.020 |
| J0119* | yes | 8 | 0.001 | 0.005 | ... | 0.024 | 0.068 | 0.060 | 0.008 | . . | . . | 0.022 | ... | ... |
| J0132* | yes | 11 | 0.007 | 0.004 | ... | 0.013 | 0.121 | 0.062 | 0.008 |  | . | 0.079 | $\ldots$ |  |
| K0027* | yes | 65 | 0.003 | 0.948 | 0.705 | 0.154 | 0.505 | 0.378 | 0.035 | 0.008 | $\ldots$ | ... | . . . | 0.124 |
| K0049 | yes | 53 | 0.321 | 0.652 | 0.108 | $\cdots$ | . | 0.062 | 0.177 | 0.013 | ... | 0.732 | ... | 0.002 |
| K0060** | no | 33 | ... | 0.868 | 0.129 | 0.001 | 0.235 | 0.141 | 0.006 | 0.009 | $\ldots$ | ... | ... | 0.004 |
| K0061 | yes | 65 | 0.360 | 0.566 | 0.095 | ... | . | 0.111 | 0.194 | 0.018 | . . | 1.21 | ... | 0.362 |
| K0073 | yes | 65 | 0.378 | 0.718 | 0.131 | 0.002 | 0.003 | 0.104 | 0.225 | ... | $\ldots$ | . | . . . | 0.078 |
| K0083** | yes | 81 | 0.006 | 0.354 | 0.071 | 0.010 | 0.796 | 0.515 | $\ldots$ | $\cdots$ | $\cdots$ | 0.994 | $\cdots$ | 0.059 |


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TABLE 1-Continued.

| Sample | Metallic Paint | Counting Time, s | Ca | Ti-Ka/ Ba-L Ratio |  | Cr | Mn | Cu | Zn | As-L ${ }_{\alpha} /$ <br> Pb- $\mathrm{L}_{\alpha}$ <br> Ratio | $\mathrm{Se}-\mathrm{K}_{\text {a }}$ | As-L $\mathrm{L}_{\mathrm{p}} /$ $\mathrm{Br}-\mathrm{K}_{\mathrm{a}}$ Ratio | $\begin{aligned} & \mathrm{Pb}-\mathrm{L}_{\beta} / \\ & \mathrm{Se}-\mathrm{K}_{\beta} \\ & \text { Ratio } \end{aligned}$ | Sr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L0007 | no | 323 | 0.198 | 0.164 | ... | $\ldots$ | 0.280 | 0.018 | 0.097 | . | $\ldots$ | . | 0.002 | 0.043 |
| L0021** | no | 183 | 0.004 | 0.407 | 0.028 | 0.057 | 0.076 | 0.044 | 0.005 | ... | ... | $\ldots$ | ... | 0.098 |
| L0045 | yes | 91 | 0.505 | 0.168 |  | 0.001 | 0.853 | 0.272 | 0.291 | $\ldots$ | $\ldots$ | $\ldots$ |  | 0.269 |
| L0050 | yes | 917 | 0.725 | 0.170 | $\ldots$ | ... | 0.893 | 0.059 | 0.336 | $\cdots$ | $\ldots$ | $\ldots$ | $\ldots$ | 0.626 |
| L0069 | no | 550 | 0.439 | 0.168 | ... | . $\cdot$ | 0.580 | 0.036 | 0.178 | $\ldots$ | $\ldots$ | $\cdots$ | $\ldots$ | 0.060 |
| L0098* | no | 208 | 0.003 | 0.157 | 0.018 | 0.134 | 0.174 | 0.122 | 0.031 | 0.001 | $\cdots$ | $\cdots$ |  | 0.003 |
| L0102* | no | 518 | 0.002 | 0.150 | 0.111 | 0.547 | 0.617 | 0.460 | 0.252 | ... | ... | $\ldots$ | ... |  |
| L0103** | no | 165 | 0.001 | 0.329 | 0.018 | 0.066 | 0.099 | . 0.056 | 0.011 | 0.003 | $\ldots$ | $\cdots$ | $\ldots$ | 0.045 |
| Barium-Based Paints ${ }^{\text {b }}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| B0018** | yes | 55 | 0.003 | 0.744 | 0.104 | 0.256 | 0.385 | 0.167 | 0.037 | 0.005 | $\ldots$ | $\ldots$ |  | 0.192 |
| B0020* | yes | 62 | 0.003 | 0.721 | 0.122 | 0.255 | 0.355 | 0.129 | 0.013 | ... | $\ldots$ | $\ldots$ | 0.010 | 0.202 |
| C0001** | no | 72 | 0.005 | 0.842 | 0.192 | 0.366 | 0.755 | 0.206 | 0.800 | $\cdots$ | $\ldots$ | ... | ... | 0.235 |
| C0034** | no | 47 | 0.005 | 0.852 | 0.126 | 0.176 | 0.181 | 0.216 | 0.843 | ... | $\ldots$ | 0.070 | 0.005 | 0.356 |
| E0017** | yes | 41 | $\ldots$ | 0.501 | 0.129 | 0.104 | 0.171 | 0.107 | 0.007 | $\ldots$ | $\ldots$ | ... |  | 0.301 |
| F0030** | yes | 55 | 0.002 | 0.868 | 0.128 | 0.185 | 0.529 | 0.102 | 1.03 | 0.003 | ... | ... | 0.022 | 0.404 |
| H0029** | no | 38 | 0.004 | 0.465 | 0.054 | 0.183 | 0.379 | 0.124 | 0.025 | ... | ... | 0.010 | 0.024 | 0.081 |
| K0014* | yes | 87 | 0.004 | 0.785 | 0.166 | 0.472 | 0.863 | 0.283 | 0.018 | $\ldots$ | $\ldots$ | $\ldots$ | 0.068 | 0.226 |
| K0015** | yes | 60 | ... | 0.052 | 0.133 | 0.240 | 0.786 | 0.255 | 1.02 | 0.019 | $\cdots$ | 0.988 | ... | 0.234 |
| K0016** | yes | 49 | 0.006 | 0.938 | 0.192 | 0.150 | 0.237 | 0.219 | 0.855 |  |  | 0.071 | 0.005 | 0.361 |
| K0026** | yes | 55 | ... | 0.869 | 0.127 | 0.264 | 0.482 | 0.133 | 0.731 | 0.015 | $\ldots$ | 0.096 | 0.027 | 0.268 |
| K0106* | yes | 54 | 0.006 | 0.750 | 0.117 | 0.223 | 0.804 | 0.234 | 0.062 | 0.002 | $\cdots$ | ... |  | 0.193 |
| L0004** | yes | 51 | 0.007 | 0.749 | 0.103 | 0.204 | 0.262 | 0.144 | 0.091 | 0.004 | ... | $\ldots$ | 0.016 | 0.212 |
| L0010** | yes | 63 | ... | 0.711 | 0.112 | 0.264 | 0.321 | 0.252 | 0.031 | ... | $\ldots$ | $\ldots$ | ... | 0.224 |
| L0011* | yes | 114 | ... | 0.677 | 0.186 | 0.792 | 0.920 | 0.609 | 0.047 | ... | $\ldots$ | $\ldots$ | $\cdots$ | 0.118 |
| L0022* | yes | 75 |  | 0.722 | 0.161 | 0.418 | 0.485 | 0.323 | 0.018 |  |  | $\ldots$ |  | 0.138 |
| L0023* | yes | 64 | $\ldots$ | 0.723 | 0.134 | 0.332 | 0.408 | 0.387 | 0.023 | 0.020 | $\ldots$ | $\ldots$ | $\ldots$ | 0.175 |
| Lead-Based Paints |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| E0003** | no | 51 |  | 0.010 | 0.016 | 0.100 | 0.020 | 0.028 | 0.005 | 0.063 | 1.26 | 0.014 | 0.005 | 0.028 |
| E0024** | no | 93 | 0.002 | 0.141 | 0.127 | 0.129 | 0.041 | 0.030 | 0.016 | 0.002 | 1.28 | 0.011 | 0.001 | 0.072 |
| E0046 | no | 103 | 0.011 | 0.039 | 0.014 | 0.118 | 0.018 | 0.044 | ... | 0.013 | 1.33 | 0.012 | 0.002 | 0.044 |


| E0054 | no | 200 | 0.052 | 0.071 | 0.019 | 0.137 | 0.019 | 0.091 |  | 0.046 | 1.36 | 0.009 |  | 0.024 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| E0076 | no | 132 | 0.020 | 0.031 | 0.012 | 0.123 | 0.021 | 0.040 | $\ldots$ | 0.030 | 1.33 | 0.010 | 0.001 | 0.023 |
| E0094* | no | 141 | 0.001 | 0.014 | 0.008 | 0.140 | 0.104 | 0.099 | 0.062 | 0.027 | 1.34 | 0.007 |  | 0.019 |
| E0095** | no | 234 | ... | 0.008 | 0.003 | 0.193 | 0.219 | 0.206 | 0.106 | 0.075 | 1.30 | 0.006 | 0.005 | 0.023 |
| E0096** | no | 108 | 0.002 | 0.075 | 0.071 | 0.138 | 0.046 | 0.027 | 0.019 | 0.007 | 1.32 | 0.014 | 0.005 | 0.041 |
| G0019 | no | 180 | 0.037 | 0.175 | 0.023 | 0.112 | ... | 0.409 | ... | 0.009 | 1.33 | 0.010 |  | 0.083 |
| G0056 | yes | 393 | 0.208 | 0.508 | 0.096 | 0.137 | 0.020 | 0.355 | ... | 0.130 | 1.34 | ... |  | 0.232 |
| G0070 | no | 62 | 0.002 | 0.016 | 0.003 | 0.113 | 0.018 | 0.018 | ... | 0.004 | 1.30 | 0.012 | 0.002 | 0.008 |
| G0115* | no | 138 | 0.002 | 0.095 | 0.076 | 0.150 | 0.064 | 0.909 | 0.028 | 0.008 | 1.31 | 0.010 | 0.005 | 0.036 |
| H0043 | no | 254 | 0.064 | 0.950 | 0.156 | 0.106 | 0.004 | 0.136 | ... | 0.034 | 1.32 | 0.006 | . . . | 0.025 |
| H0067 | no | 204 | 0.045 | 0.967 | 0.154 | 0.079 | 0.009 | 0.040 |  | 0.033 | 1.27 | 0.010 |  | 0.022 |

[^1]TABLE 2-Elemental distribution in the NBS 1974 Automotive Colors.

|  | Ca | Ti | Ba | Cr | Mn | Fe | Cu | Zn | As | Se | Br | Pb | Sr |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Samples, no. | 86 | 100 | 60 | 117 | 120 | 138 | 115 | 121 | 19 | 18 | 31 | 32 | 121 |
| Samples, \% | 61.4 | 71.4 | 42.8 | 83.6 | 85.7 | 98.6 | 82.1 | 86.4 | 13.6 | 12.8 | 22.1 | 22.8 | 86.4 |
| Titanium-based paints, \% | 60.7 | 100 | 35.7 | 57.1 | 64.3 | 92.8 | 78.6 | 85.7 | 3.6 | 7.1 | 14.3 | 17.8 | 85.7 |
| Barium-based paints, \% | 58.8 | 41.2 | 100 | 100 | 100 | 100 | 100 | 100 | 14.3 | 0 | 35.7 | 0 | 100 |
| Iron-based paints, \% | 48.8 | 68.8 | 31.2 | 87.5 | 90 | 100 | 87.5 | 82.5 | 11.2 | 3.8 | 35 | 13.8 | 82.0 |
| Lead-based paints, \% | 85.7 | 85.7 | 57.1 | 100 | 92.8 | 100 | 42.8 | 100 | 57.1 | 92.8 | 57.1 | 100 | 100 |



FIG. 1-Diagram of the determination by computer of area and background counts for titanium $K_{a}$ peak at 100-II.
background as possible. The criteria were readily met in the calcium through copper region of the spectrum. The bremsstrahlung region, however, required division of the background into four regions favoring the elements in each division. The specifications for the peak spans are listed in Table 3.
It is important to note that peak area count is not based solely on the peak span of the specified elemental peak. The varying altitudes of the right and left spans, especially in the bremsstrahlung region, are troublesome. In the preliminary assignments of the peak spans, an attempt was made to establish the optimum right and left spans to minimize the extreme variation of peaks with a high signal to noise ratio. All the preceding operating conditions were entered into the minicomputer's memory core, and the analyses of the paint samples were initiated by the developed program.

## Results

All paint samples were analyzed in reference to their predominant element. The program for each category used the same net ratios and was devised to limit the analysis of each sample to a preset number of counts for the respective base elemental peak. The

TABLE 3-Elemental peak spans incorporated into the general paint analysis program (all peaks listed are $K_{\alpha}$ unless otherwise stated).

| Peak | Right Span | Left Span |
| :---: | :---: | :---: |
| 1, Ca 75-11 | 193-6 | 70-6 |
| 2. $\mathrm{Ti} 100-11 \mathrm{Ba}-\mathrm{L}_{a}$ | 193-6 | 70-6 |
| 3. $\mathrm{Ba}-\mathrm{L}_{\beta} 113-11$ | 193-6 | 70-6 |
| 4. $\mathrm{Cr} 126-11 \mathrm{Ba}-\mathrm{L}_{\gamma} 130-4$ | 193-6 | 70-6 |
| 5. Mn 140-11 | 193-6 | 70-6 |
| 6. Fe 155-11 | 193-6 | 70-6 |
| 7. $\mathrm{Cu} 203-11$ | 290-3 | 168-6 |
| 8. $\mathrm{Zn} 220-11$ | 290-3 | 168-6 |
| 9. As 275-11 Pb-L ${ }_{\alpha}$ | 290-3 | 193-6 |
| 10. Se 294-11 | 365-4 | 260-3 |
| 11. As-K ${ }_{\beta} 309-11 \mathrm{Br} 314-11$ | 365-4 | 260-3 |
| 12. $\mathrm{Pb}-\mathrm{L}_{\beta} 335-11 \mathrm{Se}-\mathrm{K}_{\beta} 332-11$ | 365-4 | 260-3 |
| 13. $\mathrm{Sr} 380-11$ | 446-4 | 365-4 |

elemental peaks chosen to represent these elements were the iron $K_{\alpha}$, titanium $K_{\alpha}$, barium $\mathrm{L}_{\alpha}$, and lead $\mathrm{L}_{\beta}$ peaks. This approach allows specimens of different sample size to be compared directly. In a few cases, the base element was in such high concentration that the analysis was completed in less than 10 s ; in other instances 600 to 1500 s were required to complete the analysis.

A 600 -s analysis is statistically more acceptable than a $10-\mathrm{s}$ analysis, but the latter is not without value even though it has a larger statistical range. The longer analysis times were unusual in the large paint population studied, which required an average analysis time of 114 s . The statistical importance for each count of an analysis is dependent on a large number of variables because of drift in instrumental components and operating conditions. Specifically, these include X-ray tube potential and current, intensity and distribution of X-ray emissions, detector's electronic noise, and ADC dead time instabilities [7].

The statistical range considered for any single count is $(N \pm 2 \sqrt{N}) /\left(N^{\prime} \pm 2 \sqrt{N^{\prime}}\right)$ where $N$ is any elemental count considered and $N^{\prime}$ is the base elemental count. For replicate analyses the statistical range is $\bar{N}$ and $\bar{N}^{\prime}$, with the $2 \sigma$ value applied as above. ${ }^{2}$ The point scatter for each element is considered to be within two standard deviations of the true value or the quality of statistical precision expresses a $95 \%$ confidence level [2,Sec. 3.3(a)].
The approach was inadequate for low count rates; therefore, after further experimentation, we found that a questioned elemental count could be verified by submitting a sample to replicate analysis. A minimum of three runs was conducted to average a low count, calculate a $2 \sigma$ value, and observe whether any single count exceeded the range. If the counts exceeded the range intermittently, it was considered that the background varied to the point that the element's presence could not be confirmed.

## System Stability

The stability of the system was examined before the comparative analyses were tabulated. Three samples were analyzed $21 / 2$ months after the original analyses. Repeatability of results using the ratio technique was excellent.

[^2]
## Homogeneity of Paint Samples

Paint samples being compared elementally must be homogeneous within a batch formulation for the analysis to have any significance. Taking selected samples, analyses were conducted with a molybdenum minicollimator to limit the analysis area on three positions approximately 20 mm apart on each paint chip. In all samples, the ratio ranges were within the defined $2 \sigma$ values. Table 4 and Fig. 2 illustrate the homogeneity of Sample 74E0003.


FIG. 2-Graph showing the homogeneity of sample constituents for Positions 1, 2, and 3 for Sample 74E0003.

TABLE 4-Homogeneity of sample constituents as shown by range of ratios for Sample 74E0003.

| Element | Position 1 |  | Position 2 |  | Position 3 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | High | Low | High | Low | High | Low |
| Ca | 0.002 | 0.001 | 0.002 | 0.001 | 0.000 | 0.000 |
| $\mathrm{Ti}_{\alpha}$ | 0.014 | 0.012 | 0.017 | 0.015 | 0.016 | 0.013 |
| $\mathrm{Ti}_{\beta}$ | 0.020 | 0.016 | 0.020 | 0.017 | 0.022 | 0.019 |
| Cr | 0.103 | 0.096 | 0.102 | 0.094 | 0.110 | 0.101 |
| Mn | 0.022 | 0.019 | 0.025 | 0.021 | 0.024 | 0.020 |
| Fe | 0.035 | 0.030 | 0.035 | 0.030 | 0.034 | 0.030 |
| Cu | 0.007 | 0.005 | 0.005 | 0.004 | 0.008 | 0.006 |
| Zn | 0.050 | 0.042 | 0.056 | 0.050 | 0.058 | 0.057 |
| $\mathrm{Pb}_{\alpha}$ | 1.28 | 1.22 | 1.25 | 1.20 | 1.27 | 1.22 |
| Se | 0.016 | 0.013 | 0.017 | 0.014 | 0.018 | 0.015 |
| $\mathrm{As}_{\beta}$ | 0.004 | 0.003 | 0.005 | 0.004 | 0.004 | 0.003 |
| $\mathrm{Pb}_{\beta}$ | base | base | base | base | base | base |
| Sr | 0.032 | 0.028 | 0.028 | 0.021 | 0.029 | 0.025 |

## Homogeneity of Similarly Catalogued Paints from Different NBS Collections

Because two sets of the NBS Automotive Colors were available, the authors were able to analyze selected samples from different collections. Three samples (74E0068, 74E0003, 74A0044) from each set were analyzed and their net ratios were compared; in general, the ratios overlapped. In the cases where overlap did not occur, the $2 a$ values were within 5 to $10 \%$ of the lower ratio; although these small differences exist, the paint samples most probably have the same elemental profile.

## Comparison of Similarly Colored Paints

The paint samples were compared visually for similar color and metallic flaking. Table 5 lists the samples that had similar colors. The samples were removed from their plastic folders for easy overlay, placed on a dull white background, and compared under indirect sunlight. They were also observed on the stage of a stereobinocular microscope at $\times 7$ to $\times 30$.

The categories that were chosen to be displayed in graphic form were generally the largest populations. The colors of the paints in each category were not exact matches, and slight variations in the texture of the metallic flaking were also observed, but samples were not excluded on that basis. Figures 3-8 and Tables 6-11 illustrate the elemental profiles of similarly colored paint samples from randomly selected categories. Visually similar samples in each color class are easily separated by their elemental composition with the exception of those samples in Fig. 8 and Table 11.

Comparison of the paints was usually based on a single analysis, as the repeatability of the system permitted the observation of gross elemental differences. Where only minor differences were observed, replicate analyses were made. If the samples were not discriminated it was necessary to go "off program" and to analyze the samples for their total elemental profile. It is important to note that the twelve element program is a method of elimination, as illustrated in Figs. 3-8 and Tables 6-11. Additional analyses should be conducted before paint samples of similar elemental composition are reported as being physically and chemically the same.

A common consideration in the analysis of paint by EDX is the introduction of interfering elements from undercoat layers and any supporting backing. The presence of aluminum backing on samples in this study caused elevated levels of chromium, manganese,

TABLE 5-Paint standards from Automotive Colors that were indistinguishable by color.

White, nonmetallic flaking, Group 1
Ti A0044-see Table 6, Fig. 3
Ti A0122
Ti A0123
White, nonmetallic flaking, Group 2
Ti A0033
Ti A0121
Gray, metallic
Ti B0057
Fe B0052
Fe B0092
Fe B0129
Black, nonmetallic flaking, Group 1
Ba C0001
Ba C0034
Black, nonmetallic flaking, Group 2
Fe C0041-see Table 7, Fig. 4
Fe C 0090
Red, nonmetallic flaking
Pb E0003-see Table 8, Fig. 5
Pb E0024
Pb E0046
Pb E0054
Pb E0094
Red, metallic
Fe E0068-see Table 9, Fig. 6
Fe E0085
Fe E0130
Brown, metallic, Group 1
Fe F0012
Fe F0040
Fe F0127
Fe F0133

Brown, metallic, Group 2
Fe F0032
Fe F0074
Fe F0111
Fe F0126
Brown, metallic, Group 3
Fe F0013
Fe F0110
Brown, metallic, Group 4
Fe F0038
Fe F0139
Brown, metallic, Group 5
Fe F0128
Fe F0134
Yellow, nonmetallic flaking, Group 1
Ti H0008
Ti H0037
Yellow, nonmetallic flaking, Group 2
Ti H0035-see Table 10, Fig. 7
Ti H0079
Green, metallic
Ba K0106
Fe K0061
Blue, metallic, Group 1
Fe L0124
Fe L0131
Blue, metallic, Group 2
Fe L0100-see Table 11, Fig. 8
Fe L0135
iron, and zinc. In fact, most of the samples tabulated in Table 2 contain these elements. The increases so introduced were observed to be on the order of 0.010 to 0.060 of the base elements, significant enough to alter the paint specimen's elemental profile but not enough to interfere with programmed analysis. Net ratios are low enough to allow stripping of the aluminum spectrum from the paint spectrum, thus eliminating interferences introduced by the backing. Interelement effects due to the aluminum backing are insignificant and do not interfere with comparative analysis of the paint samples.

## Conclusion

It is evident to those observing the qualitative and semiquantitative compositions of the 1974 U.S. automotive paints that certain elements are common to many paints in a sufficiently wide variety of concentrations to discriminate among similarly colored samples.

Perhaps one of the most crucial aspects considered in the study was the homogeneity of the elemental components of the paint panels. Samples were found to be homogeneous within themselves and among panels prepared from the same paint source. In an approximation of real-case situations, paint specimens were subjected to analyses identical to routine paint analysis in a forensic laboratory.

In only two instances were the authors unable to discriminate by programmed analysis


FIG. 3-Graph of the range of ratios for three, white, titanium-based paint samples (see Table б).

TABLE 6-Range of ratios for three, white, titanium-based paint samples (see Fig. 3).

|  | Range of Ratios |  |
| :--- | :---: | :---: |
| Element | High | Low |
|  | A0044 |  |
| Ca | 0.054 |  |
| Ti | base | 0.048 |
| Ti | base |  |
| Mn | 0.169 | 0.158 |
| Fe | 0.006 | 0.003 |
| Cu | 0.050 | 0.045 |
| Zn | 0.019 | 0.014 |
| Sr | 0.031 | 0.027 |
|  | 0.016 | 0.011 |
| Ti | A 0122 |  |
| Ti | base |  |
| Cr | 0.174 | base |
| Mn | 0.006 | 0.162 |
| Fe | 0.043 | 0.004 |
| Cu | 0.064 | 0.038 |
| Zn | 0.053 | 0.058 |
| Pb | 0.028 | 0.047 |
| Pb | 0.008 | 0.024 |
| Sr | 0.003 | 0.006 |
|  | 0.012 | 0.002 |
|  | A 0123 | 0.010 |
| Ca | 0.005 |  |
| Ti | base | 0.003 |
| Ti | 0.164 | base |
| Cr | 0.017 | 0.152 |
| Mn | 0.068 | 0.014 |
| Fe | 0.101 | 0.062 |
| Cu | 0.060 | 0.093 |
| Zn | 0.049 | 0.054 |
| Sr | 0.004 | 0.044 |
|  | 0.003 |  |

${ }^{a}$ This sample had an aluminum-copper backing applied to it so that the three samples could be compared uniformly.


FIG. 4-Graph of the range of ratios for two, black, iron-based paint samples (see Table 7).

TABLE 7-Range of ratios for two, black, iron-based paint samples (see Fig. 4).

|  | Range of Ratios |  |
| :---: | :---: | :---: |
| Element | High | Low |
|  | C0041 |  |
| Ca | 0.832 |  |
| Ti | 0.723 | 0.786 |
| $\mathrm{Ti}_{\beta}$ | 0.165 | 0.688 |
| Mn | 0.197 | 0.129 |
| Fe | base | 0.145 |
| Cu | 0.294 | base |
| Zn | 0.720 | 0.262 |
| As | 0.007 | 0.652 |
| Sr | 0.200 | 0.003 |
|  | C 0090 | 0.154 |
| Cr | 0.153 |  |
| Mn | 0.780 | 0.121 |
| Fe | base | 0.680 |
| Cu | 0.534 | base |
| Zn | 0.193 | 0.458 |
| As | 0.009 | 0.160 |
| Sr | 0.035 | 0.004 |
|  |  | 0.022 |

${ }^{a}$ This sample had an aluminum-copper backing applied to enable uniform comparison.
between similarly colored paint samples from known sources. Paint samples E0024 and E0094 were similar when analyzed by the general program; when studied "off program," the two samples were shown to contain molybdenum. However, the respective net ratio differences established that the paint samples were not of a common origin (Fig. 5 and Table 8). Paint specimens L0100 and L0135 exhibited similar elemental compositions. Replicate "off program" and organic analyses indicated that the samples were from a common origin (Fig. 8 and Table 11). Manufacturer's information as outlined in Section 1 of Automotive Colors and information from NBS confirmed the samples' common origin.

## Summary

Elemental, qualitative, and semiquantitative analyses of 1974 U.S. automotive paints by a Finnigan Model 900F Energy Dispersive X-ray (EDX) Spectrometer are examined. This EDX analytical system incorporates a minicomputer to receive, store, and present data. The paint samples were received from the National Bureau of Standards (NBS) Law Enforcement Standards Laboratory as a collection representative of the top coats used on all U.S. manufactured automobiles in 1974.

Aspects considered include EDX system stability, homogeneity of similarly catalogued samples from different NBS collections, categorization of paints by predominant constituents, and comparison of data on paint standards that were similar.

Automated analysis represents an important application of forensic science to the characterization of paint samples and provides for the nondestructive analysis of a variety of materials in a large range of sample sizes and concentrations.


FIG. 5-Graph of the range of ratios for five, red, lead-based paint samples (see Table 8).

TABLE 8-Ranges of ratios for five, red, lead-based paint samples (see Fig. 5). ${ }^{\text {a }}$

| Element | Range of Ratios |  |
| :---: | :---: | :---: |
|  | High | Low |
| E0003 |  |  |
| Mn | 0.110 | 0.102 |
| Fe | 0.019 | 0.014 |
| Cu | 0.023 | 0.018 |
| $\mathrm{Pb}_{a}$ | 1.36 | 1.26 |
| Se | 0.019 | 0.015 |
| $\mathrm{Pb}_{\beta}$ | base | base |
| E0024 |  |  |
| Ti ${ }_{\alpha}$ | 0.018 | 0.013 |
| Cr | 0.132 | 0.125 |
| $\mathbf{M n}$ | 0.018 | 0.014 |
| $\mathrm{Pb}_{\text {a }}$ | 1.36 | 1.26 |
| Se | 0.019 | 0.014 |
| $\mathrm{Pb}_{\beta}$ | base | base |
| Mo | 0.099 | 0.092 |
| E0046 |  |  |
| Ca | 0.013 | 0.010 |
| Ti | 0.042 | 0.037 |
| $\mathrm{Ti}_{\boldsymbol{\beta}}$ | 0.016 | 0.013 |
| Cr | 0.123 | 0.113 |
| Mn | 0.019 | 0.016 |
| Fe | 0.047 | 0.042 |
| Zn | 0.015 | 0.012 |
| $\mathrm{Pb}_{\text {。 }}$ | 1.36 | 1.31 |
| Se | 0.013 | 0.011 |
| $\mathrm{As}_{\beta}$ | 0.002 | 0.002 |
| $\mathrm{Pb}_{\beta}$ | base | base |
| Sr | 0.047 | 0.042 |
| E0054 |  |  |
| Ca | 0.055 | 0.049 |
| Ti | 0.075 | 0.068 |
| $\mathrm{Ti}_{\beta}$ | 0.021 | 0.018 |
| Cr | 0.143 | 0.132 |
| Mn | 0.020 | 0.017 |
| $\mathrm{Fe}^{\text {b }}$ | 0.095 | 0.087 |
| Zn | 0.049 | 0.043 |
| $\mathrm{Pb}_{\boldsymbol{\alpha}}$ | 1.39 | 1.34 |
| Se | 0.010 | 0.007 |
| $\mathrm{Pb}_{\boldsymbol{\beta}}$ | base | base |
| Sr | 0.026 | 0.022 |
| E0094 |  |  |
| Ti ${ }_{\boldsymbol{a}}$ | 0.016 | 0.012 |
| Cr | 0.135 | 0.116 |
| Mn | 0.021 | 0.017 |
| $\mathrm{Pb}_{\text {a }}$ | 1.36 | 1.30 |
| Se | 0.018 | 0.014 |
| $\mathrm{Pb}_{\beta}$ | base | base |
| Mo | 0.071 | 0.065 |

[^3]

FIG. 6-Graph of the range of ratios for three, red, iron-based paint samples (see Table 9).

TABLE 9—Range of ratios for three, red, iron-based paint samples (see Fig. 6).

|  | Range of Ratios |  |
| :---: | :---: | :---: |
| Element | High | Low |
|  | E0068 |  |
| Ca | 0.220 |  |
| Ti | 0.349 | 0.178 |
| $\mathrm{Ti}_{\beta}$ | 0.068 | 0.293 |
| Mn | 0.075 | 0.049 |
| Fe | base | 0.045 |
| Cu | 0.070 | base |
| Zn | 0.126 | 0.050 |
| Sr | 0.066 | 0.098 |
|  | E 0085 | 0.050 |
| Ti | 0.272 |  |
| Ti | 0.045 | 0.225 |
| Cr | 0.014 | 0.030 |
| Mn | 0.507 | 0.07 |
| Fe | base | 0.434 |
| Cu | 0.247 | base |
| Pb | 0.038 | 0.203 |
| Sr | 0.027 | 0.025 |
|  | E 0130 | 0.017 |
| Cr | 0.081 |  |
| Mn | 0.420 | 0.059 |
| Fe | base | 0.356 |
| Cu | 0.241 | base |
| Zn | 0.029 | 0.197 |
| Sr | 0.035 | 0.018 |
|  |  | 0.023 |

${ }^{\text {a }}$ This sample had an aluminum-copper backing applied to enable uniform comparison.


FIG. 7-Graph of the range of ratios for two, yellow, titanium-based paint samples (see Table 10).


FIG. 8-Graph of the range of ratios for two, blue, iron-based paint samples (see Table 11).

TABLE 10-Range of ratios for two, yellow, titanium-based paint samples (see Fig. 7).

|  | Range of Ratios |  |
| :--- | :---: | :---: |
|  | High | Low |
|  | H 0035 |  |
| Ti | base | base |
| $\mathrm{Ti} \mathrm{i}_{\beta}$ | 0.306 | 0.289 |
| Cr | 0.014 | 0.012 |
| Mn | 0.096 | 0.088 |
| Fe | 0.222 | 0.208 |
| Cu | 0.069 | 0.063 |
| Zn | 0.003 | 0.002 |
| Pb | 0.002 | 0.001 |
| Sr | 0.050 | 0.045 |
|  | H 0079 |  |
| Ca | 0.021 | 0.017 |
| Ti | base | base |
| Ti | 0.125 | 0.115 |
| Fe | 0.038 | 0.034 |

TABLE 11-Range of ratios for two, blue, iron-based paint samples (see Fig. 8).

|  | Range of Ratios |  |
| :--- | :---: | :---: |
| Element | High | Low |
|  | L0100 |  |
| Ti | 0.013 |  |
| $\mathrm{Ti}_{\beta}$ | 0.004 | 0.006 |
| Cr | 0.297 | 0.001 |
| Mn | 1.01 | 0.246 |
| Fe | base | 0.889 |
| Cu | 0.745 | base |
| Zn | 0.278 | 0.643 |
| $\mathrm{As}_{\beta}$ | 0.006 | 0.230 |
| Sr | 0.016 | 0.002 |
|  | L0135 | 0.008 |
| Ca | 0.011 |  |
| Ti | 0.029 | 0.005 |
| Ti | 0.020 | 0.018 |
| Cr | 0.348 | 0.011 |
| Mn | 1.02 | 0.292 |
| Fe | base | 0.898 |
| Cu | 0.722 | base |
| Zn | 0.274 | 0.627 |
| Sr | 0.029 | 0.226 |

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[^0]:    Presented at the 46th Semiannual Meeting of the California Association of Criminalists, Fresno, Calif., 10-12 Oct. 1975. Received for publication 14 Oct. 1975; revised manuscript received 12 Jan. 1976; accepted for publication 16 Jan. 1976.
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[^1]:    ${ }^{\text {a }}$ EDX conditions: 4000 counts $\mathrm{Fe}\left(\mathrm{K}_{\sigma}\right) ; 34.0 \mathrm{kV} ; 3.00 \mathrm{~mA}$; rhodium filter; indium collimator; air path; and dead time, approximatley 35 to $40 \%$. Samples: single asterisk ( ${ }^{*}$ ) indicates aluminum panels with electrolytically deposited copper; double asterisk $\left({ }^{* *)}\right.$ indicates aluminum panel. If $\mathrm{K}_{\beta} / \mathrm{K}_{a}$ of $\mathrm{Ti}>0.165$, then Ba is present; if $\mathrm{K}_{\beta} / \mathrm{K}_{\mu}$ of $\mathrm{Ti}<0.730$,
    ${ }^{b} \mathrm{As}-\mathrm{L}_{\alpha} / \mathrm{Pb}-\mathrm{L}_{\alpha}, \mathrm{As}-\mathrm{L}_{\beta} / \mathrm{Br}-\mathrm{K}_{\alpha}$, and $\mathrm{Pb}-\mathrm{L}_{\beta} / \mathrm{Se}-\mathrm{L}_{\beta}$ are emission energies which overlap with a complexity that does not allow precise extrapolation in the barium-based paints.

[^2]:    ${ }^{2}$ Personal communication, James Mathieson, Finnigan Corp.

[^3]:    ${ }^{\text {a }}$ Samples were removed from their respective backings to enable uniform comparison.
    ${ }^{b}$ Copper and $\mathrm{As}_{\beta}$ were not present.

